

Costruiamo un semplice rosmetro

Un apparecchio facile da realizzare e utilissimo nella stazione del CB e del radioamatore

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Capita spesso di sentire un radioamatore lamentarsi delle difficoltà incontrate nel bilanciamento di un rosmetro auto-costruito. Questa taratura richiede la regolazione di piccoli condensatori nei bracci FWD e REF del ponte per ottenere correnti identiche quando, nel corso delle prove, si invertono i carichi in ingresso e in uscita. Tra le procedure di bilanciamento e di azzeramento si verificano interazioni, per cui le tarature vanno ripetute almeno due volte; in qualche caso il costernato costruttore non riesce a raggiungere il bilanciamento.

Ho ricevuto molte lettere e telefonate proprio a questo proposito. Quasi senza eccezioni il problema si rivelava dovuto a eccessive capacità minime nei compensatori di azzeramento. I radioamatori tendono a sostituire i componenti, e alla fine può capitare di montare un trimmer che non può raggiungere una capacità abbastanza bassa da consentire il bilanciamento del ponte. In condizioni ideali il compensatore dovrebbe avere, nella maggior parte dei casi, un valore variabile da 0 a 10 pF; in pratica, di solito il valore va da 3 a 10 pF e talora la capacità minima è anche superiore. Ho osservato che i compensatori a pistone in vetro hanno bassissima capacità minima, come molti variabili ad aria per montaggio su circuito stampato. I componenti

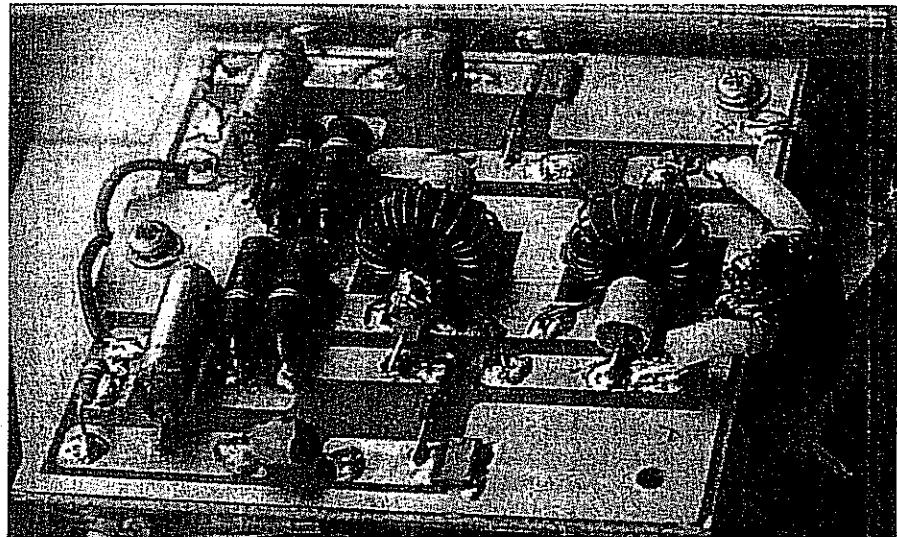


Foto A Il rosmetro di GM4ZNX.

peggiori per queste applicazioni sono quelli in plastica, ceramica o mica.

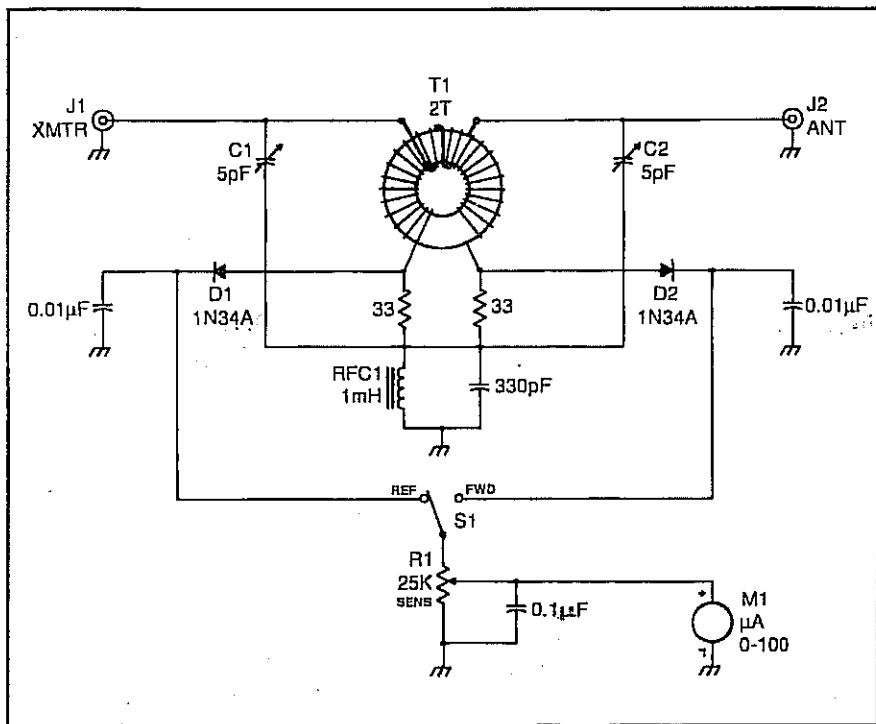
In figura 1 è riportato lo schema di un classico rosmetro che impiega compensatori di azzeramento: C1 e C2 sono i componenti incriminati.

Su un numero (Winter 1989/1990) della rivista britannica di QRP SPRAT, pubblicata dal reverendo George Dobbs, G3RJV, ho trovato un interessante schema, quasi a prova di errore, progettato da D. Stockton, GM4ZNX; il circuito è riproposto in figura 2. Ho realizzato numerose versioni del circuito di Stockton e sono sempre rimasto impressionato dal suo intrinseco bilanciamento: in questo sche-

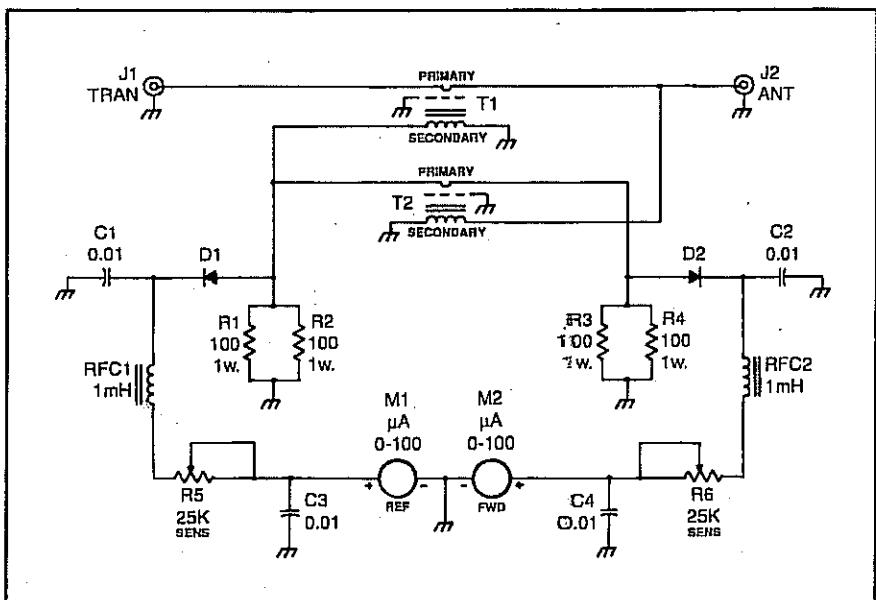
ma non occorrono compensatori. Il criterio principale di realizzazione è la disposizione dei componenti, che deve essere simmetrica; i collegamenti vanno tenuti corti e diretti.

Il circuito

Il rosmetro di figura 2 è uno strumento sensibile e con perdite di inserzione molto basse. Come nel caso del classico circuito di Warren Bruene, da cui derivano molti degli analoghi schemi attuali, il progetto di GM4ZNX non è sensibile alla frequenza: la risposta rimane essenzialmente uniforme in un intervallo operativo compreso tra 1,8 e 30 MHz. Questo non vale



1 Schema di una variante del rosmetro di Bruene, che richiede la taratura di C1 e C2 per il bilanciamento del ponte. Questo circuito è stato progettato per l'uso QRP, per cui il primario di T1 è a due spire.



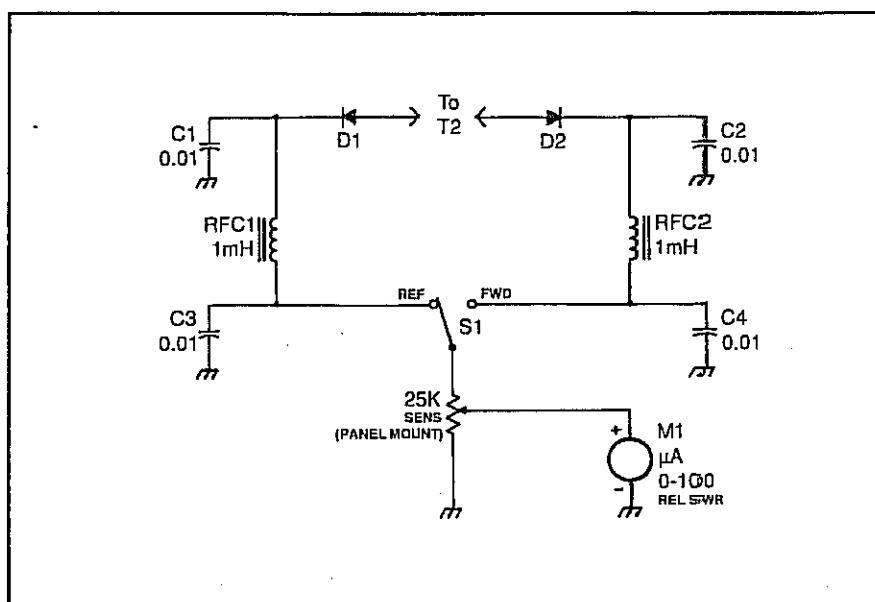
2 Schema del rosmetro di GM4ZNX. A differenza del circuito di figura 1, non richiede condensatori di bilanciamento e usa due trasformatori invece di uno. I condensatori sono ceramici a disco; le capacità sono espresse in microfarad, le resistenze in ohm. RFC1 e RFC2 sono impedanze miniatura per RF. T1 e T2 sono formati da 20 spire di filo di rame smaltato da 0,4 mm per potenze fino a 1 kW; per l'uso QRP avvolgete 12 spire di filo da 0,5 mm; i nuclei sono toroidi Amidon in ferrite FT-50-61 per l'uso da 3,5 a 30 MHz oppure FT-50-43 da 1,8 a 30 MHz. M1 e M2 sono strumenti da 100 μ A DC f.s. (vedere testo).

per i primi rosmetri Monimatch, la cui sensibilità aumentava al crescere della frequenza.

Il nostro schema può essere adattato sia per l'uso QRP sia per quello QRO. La sensibilità è determinata dal rapporto tra gli avvolgimenti dei due trasformatori. Nel WIFB's *Design Notebook*, edito dalla ARRL, ho erroneamente riferito che occorreva modificare il rapporto delle spire di uno dei due trasformatori per cambiare la sensibilità dello strumento; Stockton mi ha fatto rilevare l'inesattezza poco dopo la pubblicazione del libro, e ha anche specificato che D1 e D2 dovrebbero essere diodi Schottky (io avevo indicato due 1N34A nella versione QRP). In realtà io avevo avuto buoni risultati, a potenze di 100 watt e oltre, usando 1N914 selezionati, mentre per l'uso QRP gli 1N34A andavano benone.

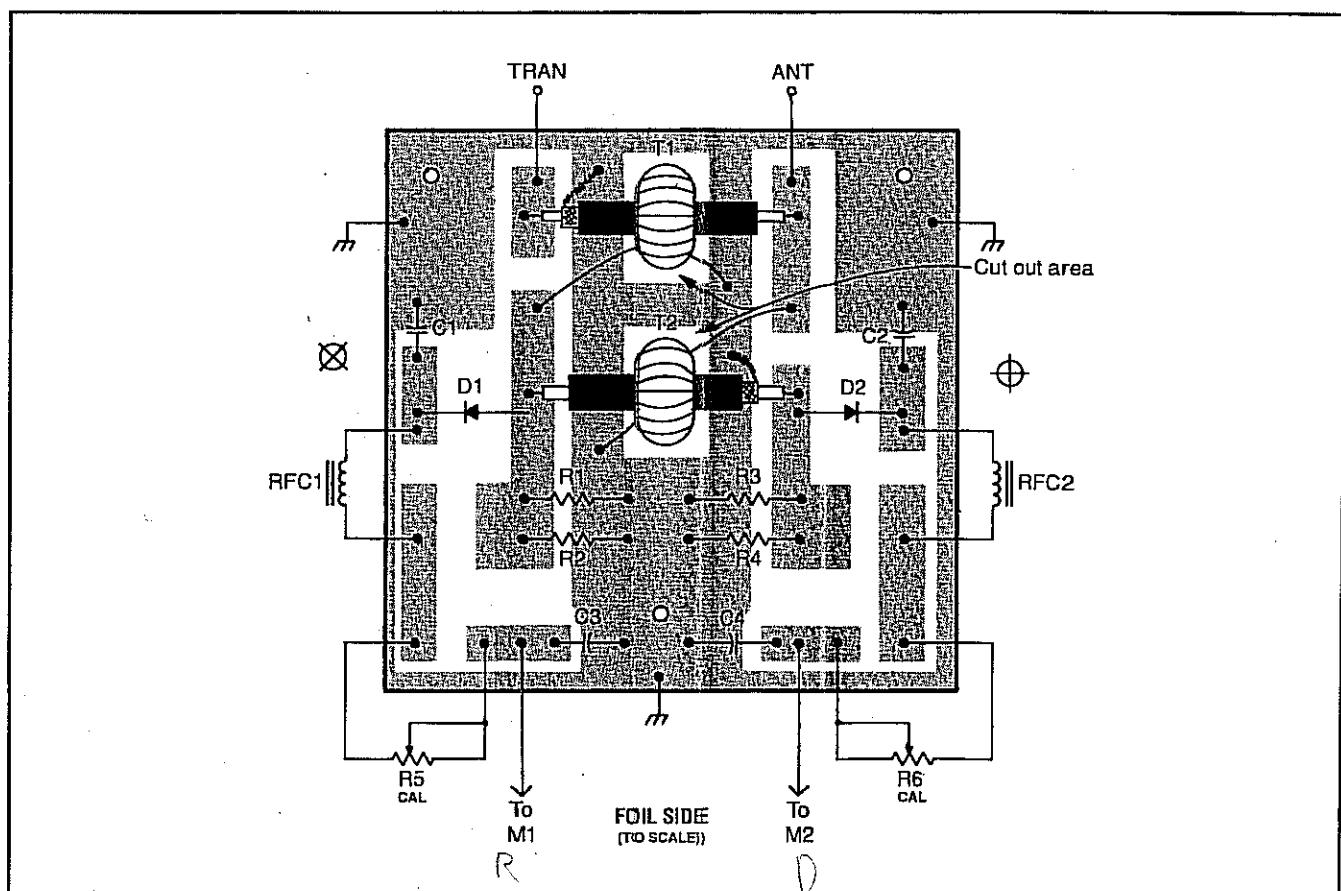
Le resistenze R1 - R4 dovrebbero essere al carbone, da 1 watt; sfortunatamente, queste resistenze non inductive al giorno d'oggi sono diventate molto rare. Le moderne resistenze al carbone sono invece costituite da un sottile strato di carbonio avvolto a spirale su un nucleo isolante e manifestano quindi una modesta ma indesiderata reattanza inductive. Non ho comunque osservato effetti negativi usando questi componenti in circuiti critici fino a 30 MHz; i problemi possono insorgere dalle VHF in su. Quindi queste resistenze spiralate si rivelano idonee per il nostro rosmetro; a ciascun punto di carico ne ho collegate in parallelo due da 100 ohm, per minimizzarne l'induttanza interna e ottenere il desiderato carico di 50 ohm.

I brevi segmenti di cavo coassiale RG-58A da 50Ω che passano attraverso i trasformatori toroidali T1 e T2 hanno la calza collegata a massa da un solo lato, come indicato nello schema: si ottiene così una schermatura di Faraday, che migliora le prestazioni del circuito.



(3) Versione con un solo strumento e deviatore FWD/REF. Per le misurazioni relative del ROS è possibile utilizzare un potenziometro di sensibilità al posto di R5 e R6.

Per il controllo simultaneo delle correnti FWD e REF si possono impiegare due strumenti separati; se preferite contenere il costo dell'apparecchio potete usare un solo indicatore e un deviatore FWD/REF. R5 e R6 vanno regolate per la deflessione a fondo scala dello strumento a un livello specificato di potenza RF; per questa calibrazione il ponte va collegato a un carico fittizio da 50Ω . Potete poi disegnare una scala graduata per vari livelli di potenza misurando la tensione RMS ai capi del carico fittizio con un voltmetro e una sonda RF ($P_{\text{Watt}} = E^2/R$) man mano che cambiate la potenza di uscita del trasmettitore. La taratura si può effettuare anche con un preciso oscilloscopio, comparandone le letture con quelle di un wattmetro RF calibrato.



(4) Circuito stampato in scala 1:1 e disposizione pratica dei componenti. I componenti vanno installati e saldati dal lato piste. Cut out area: aree di base da rimuovere per consentire l'installazione dei trasformatori toroidali.

Se siete interessati esclusivamente a una misurazione relativa del ROS potete anche evitare questa regolazione; in tal caso R5 e R6 possono essere sostituite da un potenziometro lineare da pannello da 25 kΩ. Un deviatore a levetta commuterà le linee DC FWD e REF dal ponte al deviatore e da questo al potenziometro di sensibilità (figura 3).

Gli strumenti M1 e M2 di figura 2 sono da 100 µA f.s. in corrente continua, ma vanno bene anche indicatori fino a 500 µA, tranne che nel caso di potenze QRP molto basse (inferiori a 1 watt) dove sono preferibili fondo scala da 50 o 100 µA. Io uso un economico strumento surplus da 200 µA.

Realizzazione pratica

In figura 4 è riportato il circuito stampato per il rosmetro di Stockton, che i più esperti potranno anche ridurre di dimensioni. Le piste di massa devono essere perfettamente collegate elettricamente al telaio o alla scatola dove viene installato il modulo, ad esempio tramite tre

distanziatori metallici; in questo modo si ridurranno al minimo gli effetti altrimenti induttivi delle piste di massa. Le induttanze indesiderate possono compromettere il bilanciamento del circuito.

Prove

Le prove vanno effettuate collegando il trasmettitore su J1 e un carico fittizio non induttivo da 50 Ω su J2.

Regolate la potenza di trasmissione fino a ottenere una lettura a fondo scala su M1 con il ponte commutato in modo FWD. Passate poi sulla lettura REF: su M1 deve apparire una lettura a zero. Invertite i collegamenti su J1 e J2, selezionate il modo REF e attivate il trasmettitore. M1 dovrebbe essere a fondo scala e indicare zero passando sulla posizione FWD.

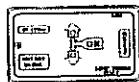
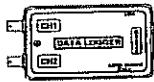
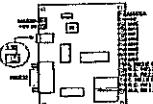
Questi risultati confermano il corretto bilanciamento del ponte. Se non li ottenete, controllate il montaggio del circuito, accertatevi di avere usato per D1 e D2 due diodi selezionati con caratteristiche perfettamente identiche e che le resistenze R1 - R4 siano esattamente da 100 Ω.

Controllate che anche T1 e T2 siano collegati esattamente come indicato in figura 2.

Considerazioni pratiche

Potete selezionare i due diodi controllandone le resistenze diretta e inversa con un ohmetro digitale. La resistenza diretta (quella più bassa) è il parametro più importante. Generalmente per i diodi 1N914 sarà compresa tra 5 e 10 Ω, mentre quella inversa supererà i 100 kΩ.

Questo strumento è il miglior rosmetro che abbia mai usato negli ultimi trent'anni: non solo è facile da costruire, ma non richiede il noioso bilanciamento necessario con gli altri strumenti. La fotografia in apertura mostra un rosmetro che ho usato per sostituire quello contenuto nel transmatch Murch MT-2000 di N8TDR: le prestazioni hanno notevolmente superato quelle dello strumento originale, che tendeva a dare indicazioni erronee su alcune bande radioamatoriali.

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THE TANDEM MATCH—AN ACCURATE DIRECTIONAL WATTMETER

Most SWR meters are not very accurate at low power levels because the detector diodes do not respond to low voltage in a linear fashion. This design uses a compensating circuit to cancel diode nonlinearity. It also provides peak detection for SSB operation and direct SWR readout that does not vary with power level. Fig 19.42 is a photo of the completed project. The following information is condensed from an article by John Grebenkemper, KI6WX, in January 1987 *QST*. Some modifications by KI6WX were detailed in the "Technical Correspondence" column of July 1993 *QST*. A PC Board is available from FAR Circuits.¹

Circuit Description

A directional coupler consists of an input port, an output port and a coupled port. Ideally, a portion of the power flowing from the input to the output appears at the coupled port, but *none* of the power flowing from the output to the input appears at the coupled port.

The coupler used in the Tandem Match consists of a pair of toroidal transformers connected in tandem. The configuration was patented by Carl G. Sontheimer and Raymond E. Fredrick (US Patent no. 3,426,298, issued February 4, 1969). It has been described by Perras, Spaulding and others. With coupling factors of 20 dB greater, this coupler is suitable to sample both forward and reflected power.

The configuration used in the Tandem Match works well over the frequency range of 1.8 to 54 MHz, with a nominal coupling factor of 30 dB. Over this range, insertion loss is less than 0.1 dB. The coupling factor is flat to within ± 0.1 dB from 1.8 to 30 MHz, and increases to only ± 0.3 dB at 50 MHz. Directivity exceeds 35 dB from 1.8 to 30 MHz and exceeds 26 dB at 50 MHz.

The low-frequency limit of this directional coupler is determined by the inductance of the transformer secondary windings. The inductive reactance should be greater than 150Ω (three times the line characteristic impedance) to reduce insertion loss. The high-frequency limit of this directional coupler is determined by the length of the transformer windings. When the winding length approaches a significant fraction of a wavelength, coupler performance deteriorates.

The coupler described here may overheat at 1500 W on 160 m (because of the high circulating current in the secondary of T2). The problem could be corrected by using a larger core or one with greater permeability. A larger core would require longer

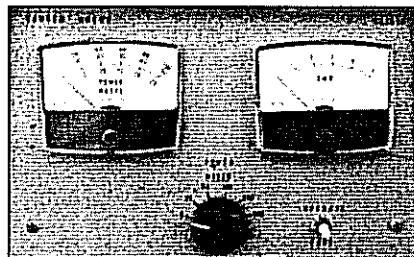


Fig 19.42—The Tandem Match uses a pair of meters to display net forward power and true SWR simultaneously.

windings; that option would decrease the high-frequency limit.

Most amateur directional wattmeters use a germanium-diode detector to minimize the forward voltage drop. Detector voltage drop is still significant, however, and an uncompensated diode detector does not respond to small signals in a linear fashion. Many directional wattmeters compensate for diode nonlinearity by adjusting the meter scale.

The effect of underestimating detected power worsens at low power levels. Under these conditions, the ratio of the forward power to the reflected power is overestimated because the reflected power is always less than the forward power. This results in an instrument that underestimates SWR, particularly as power is reduced. A directional wattmeter can be checked for this effect by measuring SWR at several power levels. The SWR should be independent of power level.

The Tandem Match uses a feedback circuit to compensate for diode nonlinearity. Transmission-line SWR is displayed on a linear scale. Since the displayed SWR is not affected by changes in transmitter power, a matching network can be simply adjusted to minimize SWR. Transmatch adjustment requires only a few watts.

Construction

The schematic diagram for the Tandem Match is shown in Fig 19.43. The circuit is designed to operate from batteries and draws very little power. Much of the circuitry is of high impedance, so take care to isolate it from RF fields. House the circuit in metal case. Most problems in the prototype were caused by stray RF in the op-amp circuitry.

The schematic shows two construction options. Connect jumpers W1, W2 and W3 to use the circuit as it was originally designed (with two 9-V batteries and TLC27L4 or TLC27M4 op amps). By

omitting these jumpers, any quad FET-input op amps can be used instead of the TLC27x4s. Possible substitutes include the TL064, TL074, TL084, LF347 and LF444. In that case you should also omit the 9-V batteries and the automatic turn-on circuitry of Q1, Q2 and Q3 (everything to the left of the jumpers on the top row of the diagram). Now you will have to connect an external + 15 V supply between the + V line and chassis ground and a -15 V supply to the -V line.

The FAR Circuits Tandem Match circuit board is double sided, but does not have plated-through holes. The component side is mainly the chassis and circuit ground planes, although there are a few signal traces. You will have to install "jumper posts" in a few locations, and solder them to both sides of the board to connect these traces. Carefully follow the schematic diagram and parts-placement diagram supplied with the board to identify these "posts." Check the board carefully to ensure that none of the ground traces pass too close to a circuit lead. You may have to scrape a bit of foil away from a few places around the component holes. This is easy with an X-ACTO knife.

The trimmer pots must be square multi-turn units with top adjustment screws for use with the FAR Circuits board. Mount the ferrite beads so they don't touch any board trace; the beads have sufficient leakage to cause problems in the high impedance parts of the circuit. Before mounting the SO-239 connectors to the circuit board, enlarge the center location holes to $\frac{1}{4}$ -inch diameter to accept the connector body. The components connected to the SO-239 are soldered directly between the center pin and the board traces.

Directional Coupler

The directional coupler is constructed in its own small ($2\frac{3}{4} \times 2\frac{3}{4} \times 2\frac{1}{4}$ -inch) aluminum box (see Fig 19.44). Two pairs of SO-239 connectors are mounted on opposite sides of the box. A piece of PC board is run diagonally across the box to improve coupler directivity. The pieces of RG-8X coaxial cable pass through holes in the PC board. (Note: Some brands of "mini 8" cable have extremely low breakdown voltage ratings and are unsuitable to carry even 100 W when the SWR exceeds 1:1. See "High-Power Operation" for details of a coupler made with RG-8 cable.)

Begin by constructing T1 and T2, which are identical except for their end connections. (Refer to Fig 19.44.) The primary for each transformer is the center conductor of a length of RG-8X coaxial cable. Cut

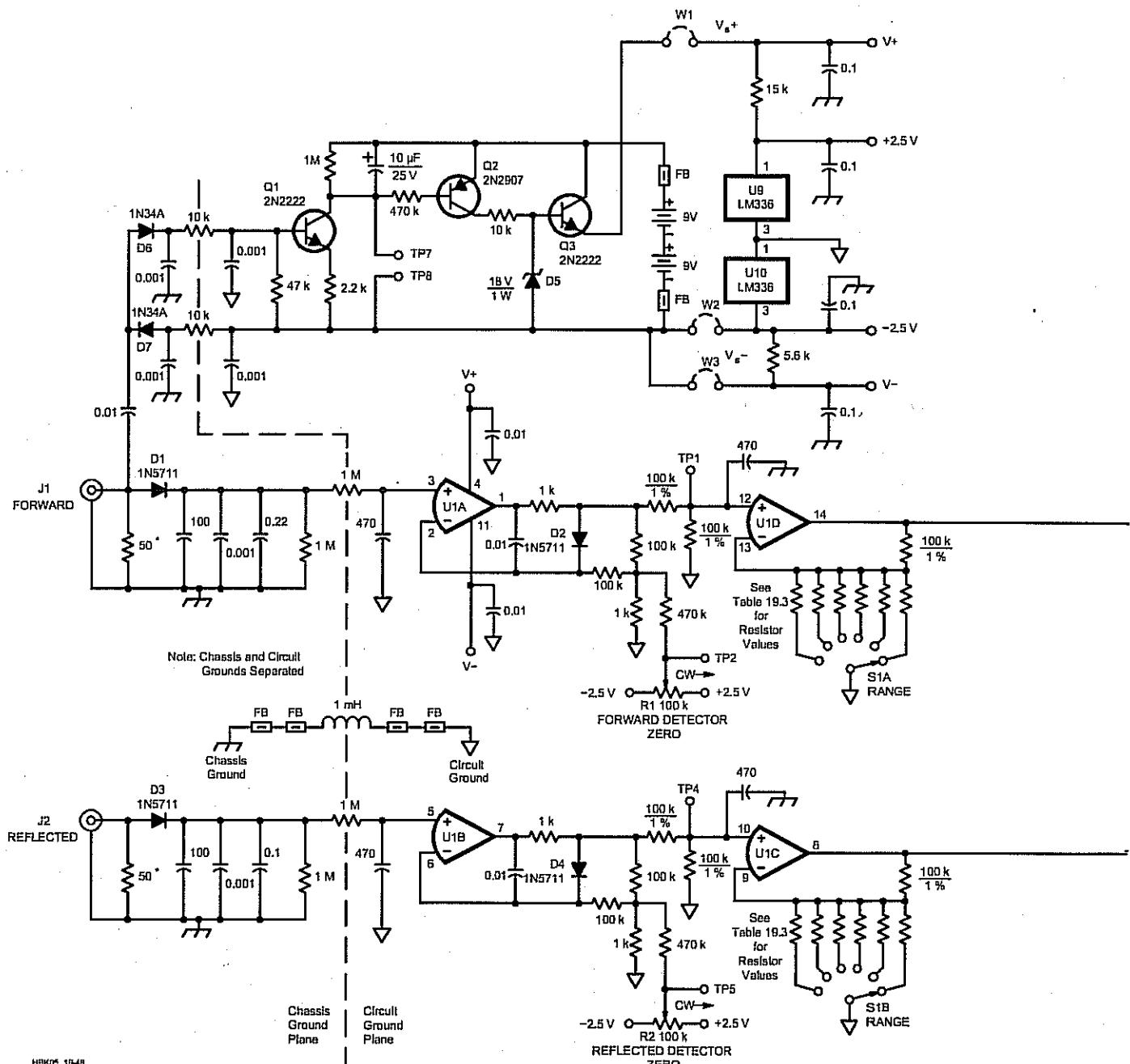


Fig 19.43—Schematic diagram of the Tandem Match directional wattmeter. Parts identified as RS are from RadioShack. Contact Information for parts suppliers can be found using the T/S Find program.

D1-D4—1N5711.

D6, D7—1N34A or 1N271.

D8-D14—1N914.

FB—Ferrite bead, Amidon FB-73-101 or equiv.

J1, J2—SO-239 connector.

J3, J4—Open-circuit jack.

M1, M2—1 mA panel meter.

Q1, Q3, Q4—2N2222 metal case only.

Q2—2N2907 metal case or equiv.

R1, R2, R5—100-k Ω , 10-turn cermet Trimpot.

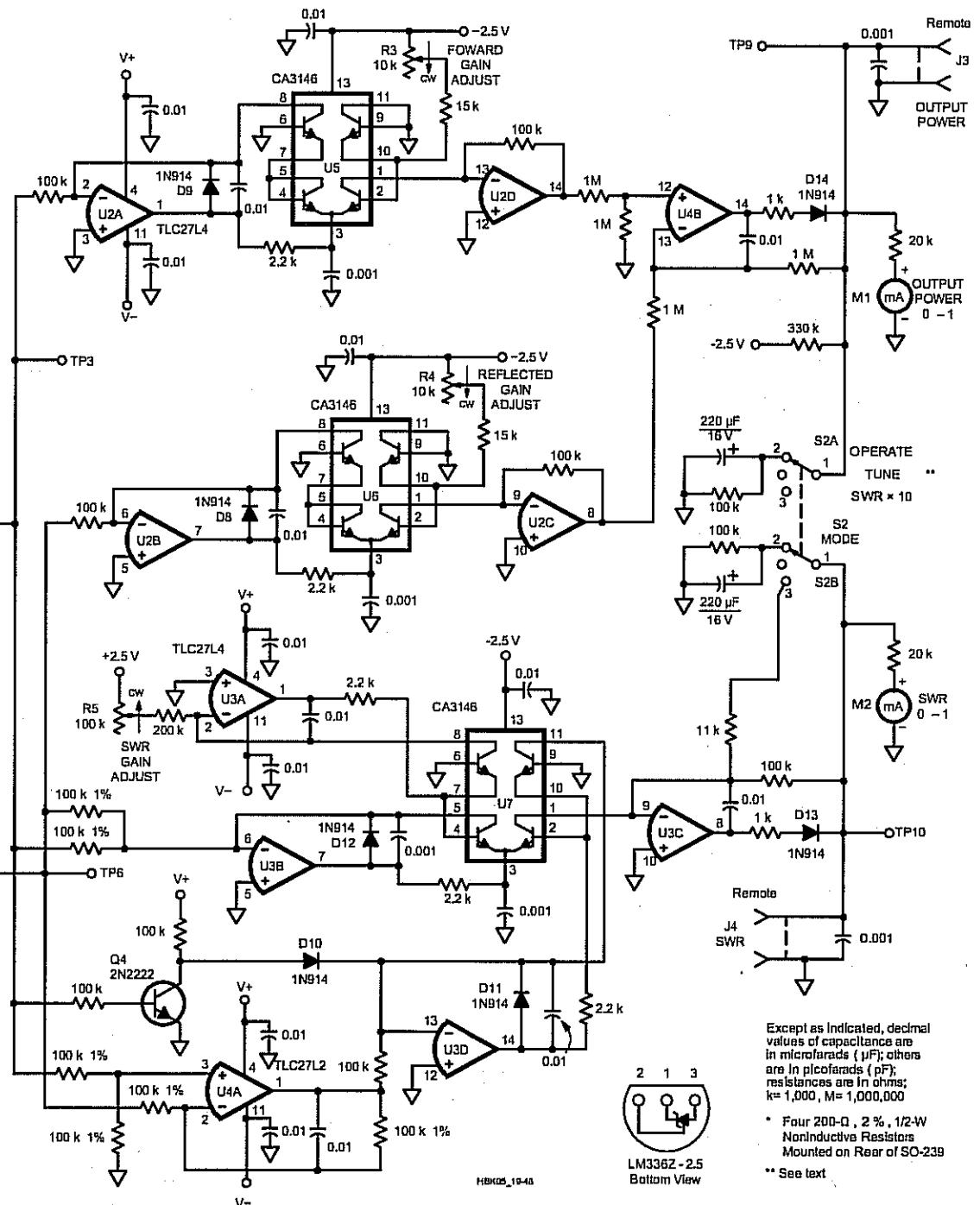
R3, R4—10-k Ω , 10-turn, cermet Trimpot.

U1-U3—TLC27M4 op amp.

U4—TLC27L2 or TLC27M2.

U5-U7—CA3146.

U9, U10—LM336.



two cable lengths sufficient for mounting as shown in the figure. Strip the cable jacket, braid and dielectric as shown. The cable braid is used as a Faraday shield between the transformer windings, so it is only grounded at one end. Impor-

tant—connect the braid only at one end or the directional-coupler circuit will not work properly! Wind two transformer secondaries, each 31 turns of #24 enameled wire on a T-50-3 iron-powder core. Slip each core over one of the prepared cable

pieces (including both the shield and the outer insulation). Mount and connect the transformers as shown in Fig 19.43, with the wires running through separate holes in the copper-clad PC board.

The directional coupler can be mounted

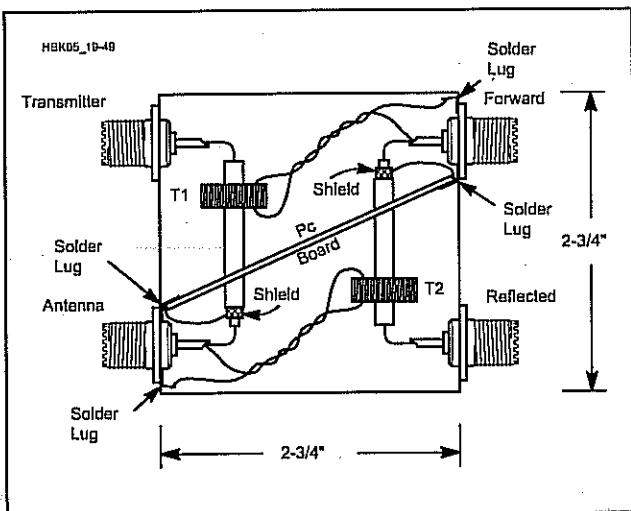


Fig 19.44—Construction details for the directional coupler. A metal case is required.

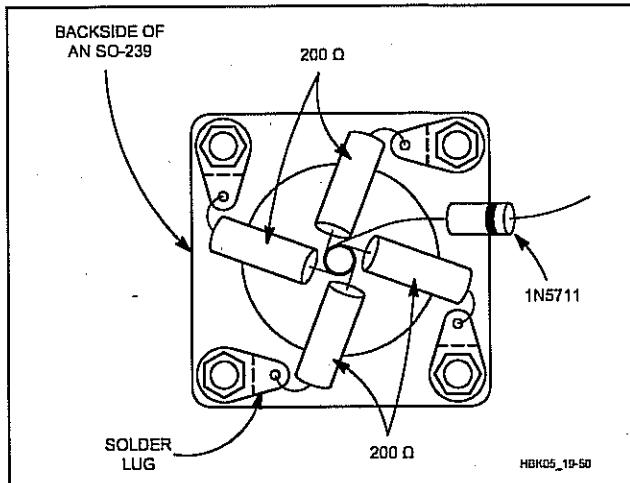


Fig 19.45—The parallel load resistors mounted on an SO-239 connector. Four 200- Ω resistors are mounted in parallel to provide a 50- Ω detector load.

separately from the rest of the circuitry if desired. If so, use two coaxial cables to carry the forward- and reflected-power signals from the directional coupler to the detector inputs. Be aware, however, that any losses in the cables will affect power readings.

This directional coupler has not been used at power levels in excess of 100 W. For more information about using Tandem Match at high power levels, see "High-Power Operation."

Detector and Signal-processing Circuits

The detector and signal-processing circuits were constructed on a perforated, copper-clad circuit board. These circuits use two separate grounds—it is extremely important to isolate the grounds as shown in the circuit diagram. Failure to do so may result in faulty circuit operation. Separate grounds prevent RF currents on the cable shield from affecting the op-amp circuitry.

The directional coupler requires good 50- Ω loads. They are constructed on the back of the female UHF chassis connectors where the cables from the directional coupler enter the wattmeter housing. Each load consists of four 200- Ω resistors connected from the center conductor of the UHF connector to the four holes on the mounting flange, as shown in Fig 19.45. The detector diode is then mounted from the center conductor of the connector to the 100-pF and 1000-pF bypass capacitors, which are located next to the connector. The response of this load and detector combination measures flat to beyond 500 MHz.

Schottky-barrier diodes (type 1N5711) were used in this design because they were readily available. Any RF-detector diode with a low forward voltage drop (less than 300 mV) and reverse breakdown voltage greater than 30 V could be used. (Germanium diodes could be used in this circuit, but performance will suffer. If germanium diodes are used, reduce the values of the detector-diode and feedback-diode load resistors by a factor of 10.)

The rest of the circuit layout is not critical, but keep the lead lengths of 0.001- and 0.01- μ F bypass capacitors short. The capacitors provide additional bypass paths for the op-amp circuitry.

D6 and D7 form a voltage doubler to detect the presence of a carrier. When the forward power exceeds 1.5 W, Q3 switches on and stays on until about 10 seconds after the carrier drops. (A connection from TP7 to TP9 forces the unit on, even with no carrier present.) The regulated references of +2.5 V and -2.5 V generated by the LM334 and LM336 are critical. Zener-diode substitutes would significantly degrade performance.

The four op amps in U1 compensate for

nonlinearity of the detector diodes. D1-D2 and D3-D4 are the matched diode pairs discussed above. A RANGE switch selects the meter range. (A six-position switch was used here because it was handy.) The resistor values for the RANGE switch are shown in Table 19.2. Full-scale input power gives an output at U1C or U1D of 7.07 V. The forward- and reflected-power detectors are zeroed with R1 and R2.

The forward- and reflected-detector voltages are squared by U2, U5 and U6 so that the output voltages are proportional to forward and reflected power. The gain constants are adjusted using R3 and R4 so that an input of 7.07 V to the squaring circuit gives an output of 5 V. The difference between these two voltages is used by U4B to yield an output that is proportional to the power delivered to the transmission line. This voltage is peak detected (by an RC circuit connected to the OPERATE position of the MODE switch) to indicate and hold the maximum power measurement during CW or SSB transmissions.

SWR is computed from the forward and reflected voltages by U3, U4 and U7. When no carrier is present, Q4 forces the

Table 19.2
Performance Specifications for the Tandem Match

- Power range: 1.5 to 1500 W
- Frequency range: 1.8 to 54 MHz
- Power accuracy: Better than $\pm 10\%$ (± 0.4 dB)
- SWR accuracy: Better than $\pm 5\%$
- Minimum SWR: Less than 1.05:1
- Power display: Linear, suitable for use with either analog or digital meters
- SWR display: Linear, suitable for use with either analog or digital meters
- Calibration: Requires only an accurate voltmeter

SWR reading to be zero (that is, when the forward power is less than 2% of the full-scale setting of the RANGE switch). The SWR computation circuit gain is adjusted by R5. The output is peak detected in the OPERATE mode to steady the SWR reading during CW or SSB transmissions.

Transistor arrays (U5, U6 and U7) are used for the log and antilog circuits to guarantee that the transistors will be well matched. Discrete transistors may be used, but accuracy may suffer.

A three-position toggle switch selects the three operating modes. In the OPERATE mode, the power and SWR outputs are peak detected and held for a few seconds to allow meter reading during actual transmissions. In the TUNE mode, the meters display instantaneous output power and SWR.

A digital voltmeter is used to obtain more precise readings than are possible with analog meters. The output power range is 0 to 5 V (0 V = 0 W and 5 V = full scale). SWR output varies from 1 V (SWR = 1:1) to 5 V (SWR = 5:1). Voltages above 5 V are unreliable because of voltage limiting in some of the op amp circuits.

Calibration

The directional wattmeter can be calibrated with an accurate voltmeter. All calibration is done with dc voltages. The directional-coupler and detector circuits are inherently accurate if correctly built. To calibrate the wattmeter, use the following procedure:

- 1) Set the MODE switch to TUNE and the RANGE switch to 100 W or less.
- 2) Jumper TP7 to TP8. This turns the unit on.
- 3) Jumper TP1 to TP2. Adjust R1 for 0 V at TP3.
- 4) Jumper TP4 to TP5. Adjust R2 for 0 V at TP6.
- 5) Adjust R1 for 7.07 V at TP3.
- 6) Adjust R3 for 5.00 V at TP9, or a full-scale reading on M1.
- 7) Adjust R2 for 7.07 V at TP6.
- 8) Adjust R4 for 0 V at TP9, or a zero reading on M1.
- 9) Adjust R2 for 4.71 V at TP6.
- 10) Adjust R5 for 5.00 V at TP10, or a full-scale reading on M2.
- 11) Set the RANGE switch to its most sensitive scale.
- 12) Remove jumpers from TP1 to TP2 and TP4 to TP5.
- 13) Adjust R1 for 0 V at TP3.
- 14) Adjust R2 for 0 V at TP6.
- 15) Remove jumper from TP7 to TP8.

This completes the calibration procedure. This procedure has been found to

Table 19.3
Range-Switch Resistor Values

Full-Scale Power Level (W)	Range Resistor (1% Precision) (kΩ)
1	2.32
2	3.24
3	4.02
5	5.23
10	7.68
15	9.53
20	11.0
25	12.7
30	15.0
50	18.7
100	28.7
150	37.4
200	46.4
250	54.9
300	63.4
500	100.0
1000	237.0
1500	649.0
2000	open

equal calibration with expensive laboratory equipment. The directional wattmeter should now be ready for use.

Accuracy

Performance of the Tandem Match has been compared to other well-known directional couplers and laboratory test equipment, and it equals any amateur directional wattmeter tested. Power measurement accuracy of the Tandem Match compares well to a Hewlett-Packard HP-436A power meter. The HP meter has a specified measurement error of less than ± 0.05 dB. The Tandem Match tracked the 436A within ± 0.5 dB from 10 mW to 100 W and within ± 0.1 dB from 1 W to 100 W. The unit was not tested above 1200 W because a transmitter with a higher power rating was not available.

SWR performance was equally good when compared to the SWR calculated from measurements made with 436A and a calibrated directional coupler. The Tandem Match tracked the calculated SWR within $\pm 5\%$ for SWR values from 1:1 to 5:1. SWR measurements were made at 8 W and 100 W.

Operation

Connect the Tandem Match in the 50-Ω line between the transmitter and the antenna-matching network (or antenna if no matching network is used). Set the RANGE switch to a range greater than the transmitter output rating and the MODE switch to TUNE. When the transmitter is keyed, the Tandem Match automatically switches on and indicates both power delivered to the antenna and SWR on the transmission line. When no carrier is present, the output power and

SWR meters indicate zero.

The OPERATE mode includes RC circuitry to momentarily hold the peak-power and SWR readings during CW or SSB transmissions. The peak detectors are not ideal, so there could be about 10% variation from the actual power peaks and the SWR reading. The SWRx10 mode increases the maximum readable SWR to 50:1. This range should be sufficient to cover any SWR value that occurs in amateur use. (A 50-ft open stub of RG-8 yields a measured SWR of only 43:1, or less, at 2.4 MHz because of cable loss. Higher frequencies and longer cables exhibit a smaller maximum SWR.)

It is easy to use the Tandem Match to adjust an antenna-matching network. Adjust the transmitter for minimum output power (at least 1.5 W). With the carrier on and the MODE switch set to TUNE or SWRx10, adjust the matching network for minimum SWR. Once minimum SWR is obtained, set the transmitter to the proper operating mode and output power. Place the Tandem Match in the OPERATE mode.

Parts

Few parts suppliers carry all the components needed for these couplers. Each may stock different parts. Good sources include Digi-Key, Surplus Sales of Nebraska, Newark Electronics and Anchor Electronics. Use the *TIS Find* program for latest address information.

High-power Operation

This material was condensed from a letter by Frank Van Zant, KL7IBA, that appears in July 1989 *QST* (pp 42-43). In April 1988, Zack Lau, W1VT, described a directional-coupler circuit (based on the same principle as Grebenkemper's circuit) for a QRP transceiver. The main advantage of Lau's circuit is very low parts count.

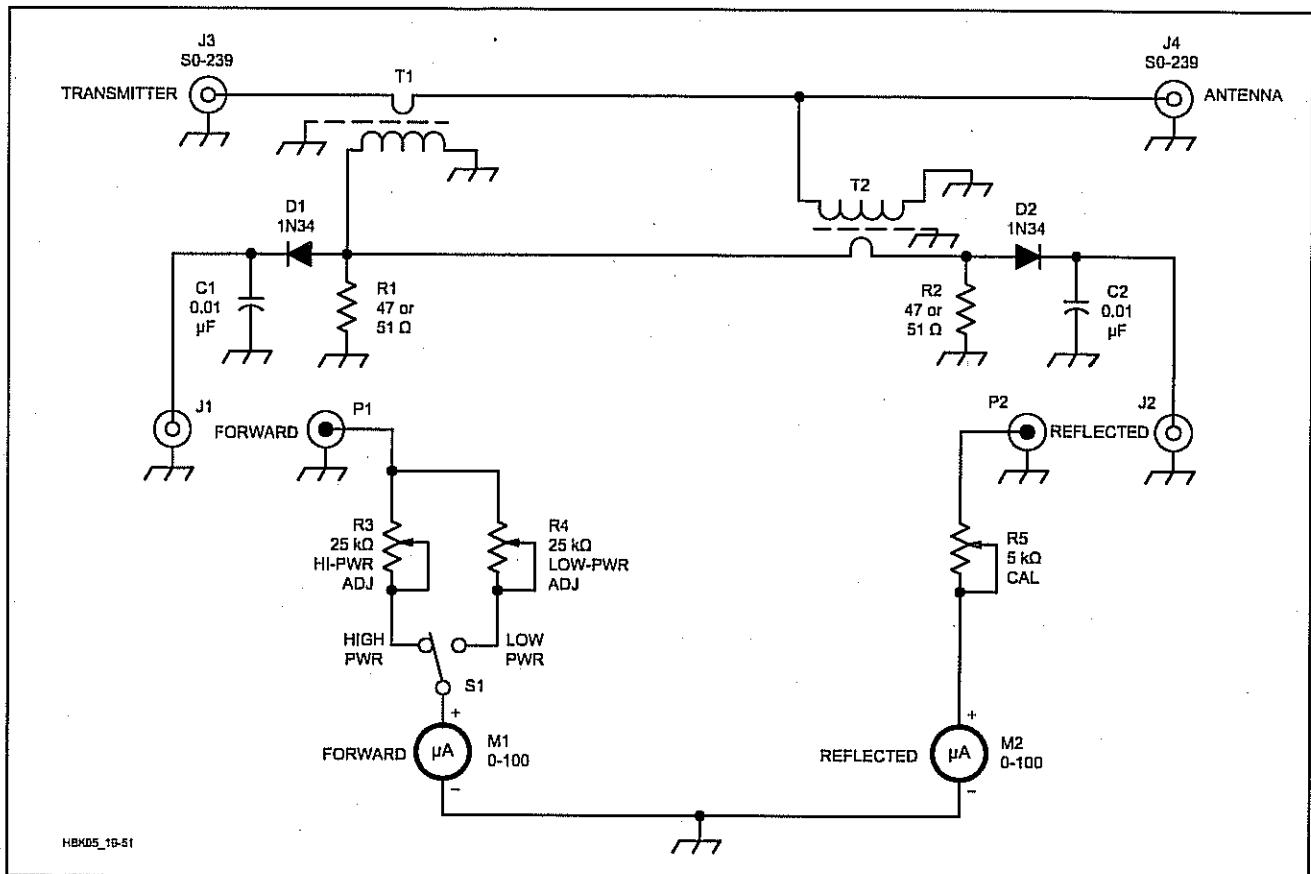
Grebenkemper uses complex log-antilog amplifiers to provide good measurement accuracy. This application gets away from complex circuitry, but retains reasonable measurement accuracy over the 1 to 1500-W range. It also forfeits the SWR-computation feature.

Lau's coupler uses ferrite toroids. It works great at low power levels, but the ferrite toroids heat excessively with high power, causing erratic meter readings and the potential for burned parts.

The Revised Design

Powdered-iron toroids are used for the transformers in this version of Lau's basic circuit. The number of turns on the secondaries was increased to compensate for the lower permeability of powdered iron.

Two meters display reflected and forward power (see Fig 19.46). The germanium



detector diodes (D1 and D2—1N34) provide fairly accurate meter readings particularly if the meter is calibrated (using R3, R4 and R5) to place the normal transmitter output at midscale. If the winding sense of the transformers is reversed, the meters are transposed (the forward-power meter becomes the reflected-power meter, and vice versa).

Construction

Fig 19.47 shows the physical layout of this coupler. The pickup unit is mounted in a 3 ½ × 3 ½ × 4-inch box. The meters, PC-mount potentiometers and HIGH/LOW power switch are mounted in a separate box or a compartment in an antenna tuner.

The primary windings of T1 and T2 are constructed much as Grebenkemper described, but use RG-8 with its jacket removed so that the core and secondary winding may fit over the cable. The braid is wrapped with fiberglass tape to insulate it from the secondary winding. An excellent alternative to fiberglass tape—with even

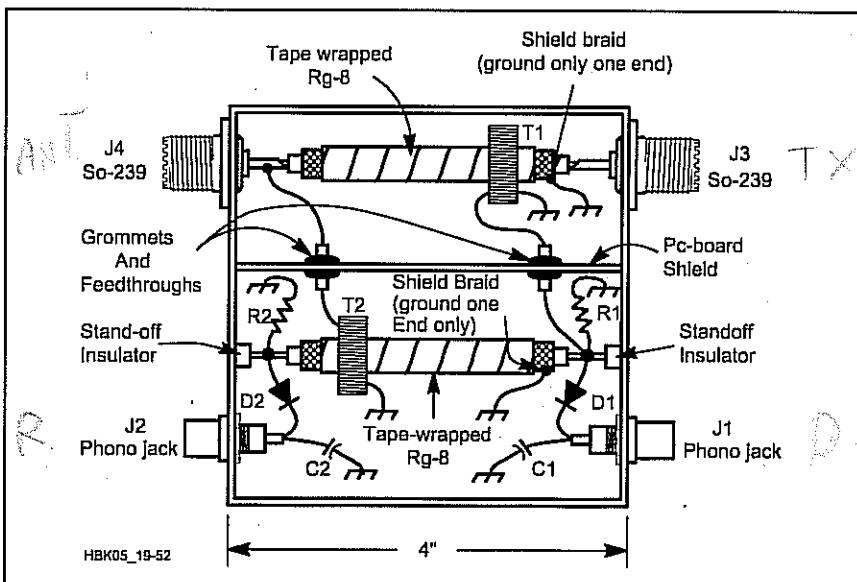


Fig 19.47—Directional-coupler construction details. Grommets or standoff insulators can be used to route the secondary windings of T1 and T2 through the PC-board shield. A 3 ½ × 3 ½ × 4-inch metal box serves as the enclosure.

higher RF voltage-breakdown characteristics—is ordinary plumber's Teflon pipe tape, available at most hardware stores.

The transformer secondaries are wound on T-68-2 powdered-iron toroid cores. They are 40 turns of #26 to 30 enameled wire spread evenly around each core. By using #26 to 30 wire on the cores, the cores slip over the tape-wrapped RG-8 lines. With #26 wire on the toroids, a single layer of tape (slightly more with Teflon tape) over the braid provides an extremely snug fit for the core. Use care when fitting the cores onto the RG-8 assemblies. After the toroids are mounted on the RG-8 sections, coat the assembly with General Cement Corp Polystyrene Q Dope, or use a spot or two of RTV sealant to hold the windings in place and fix the transformers on the RG-8 primary windings.

Mount a PC-board shield in the center of the box, between T1 and T2, to minimize coupling between transformers. Suspend T1 between SO-239 connectors

and T2 between two standoff insulators. The detector circuits (C1, C2, D1, D2, R1 and R2) are mounted inside the coupler box as shown.

Calibration, Tune up and Operation

The coupler has excellent directivity. Calibrate the meters for various power levels with an RF ammeter and a 50- Ω dummy load. Calculate I^2R for each power level, and mark the meter faces accordingly. Use R3, R4 and R5 to adjust the meter readings within the ranges. Diode nonlinearities are thus taken into account, and Grebenkemper's signal-processing circuits are not needed for relatively accurate power readings.

Start the tune-up process using about 10 W, adjust the antenna tuner for minimum reflected power, and increase power while adjusting the tuner to minimize reflected power.

This circuit has been built into several antenna tuners with good success. The

bridge worked well at 1.5-kW output on 1.8 MHz. It also worked fine from 3.5 to 30 MHz with 1.2- and 1.5-kW output. The antenna is easily tuned for a 1:1 SWR using the null indication provided.

Amplifier settings for a matched antenna, as indicated with the wattmeter, closely agreed with those for a 50- Ω dummy load. Checks with a Palomar noise bridge and a Heath Antenna Scope also verified these findings. This circuit should handle more than 1.5 kW, as long as the SWR on the feed line through the wattmeter is kept at or near 1:1. (On one occasion high power was applied while the antenna tuner was not coupled to a load. Naturally the SWR was extremely high, and the output transformer secondary winding opened like a fuse. This resulted from the excessively high voltage across the secondary. The damage was easily and quickly repaired.)

Notes

¹Use TIS Find program for latest address information.

AN EXTERNAL AUTOMATIC ANTENNA SWITCH FOR USE WITH YAESU OR ICOM RADIOS

This antenna-switching-control project involves a combination of ideas from several earlier published articles.^{1,2,3} This system was designed to mount the antenna relay box outside the shack, such as on a tower. With this arrangement, only a single antenna feed line needs to be brought into the shack. The lead photo shows the control unit and relay box, designed and built by Joe Garcia, NJ1Q. As the W1AW chief operator, Joe has plans for the switch at W1AW. Either an ICOM or Yaesu HF radio will automatically select the proper antenna. In addition, a manual switch can override the ICOM automatic selection. That feature also provides a way to use the antenna with other radios. The antenna switch is not a two-radio switch, though. It will only work with one radio at a time.

Many builders may want to use only the ICOM or only the Yaesu portion of the interface circuitry, depending on the brand of radio they own. The project is a "hacker's dream." It can be built in a variety of forms, with the only limitations being the builder's imagination.

Circuit Description

Fig 19.48 is a block diagram of the complete system. An ICOM or Yaesu HF radio connects to the appropriate decoder via the accessory connector on the back of

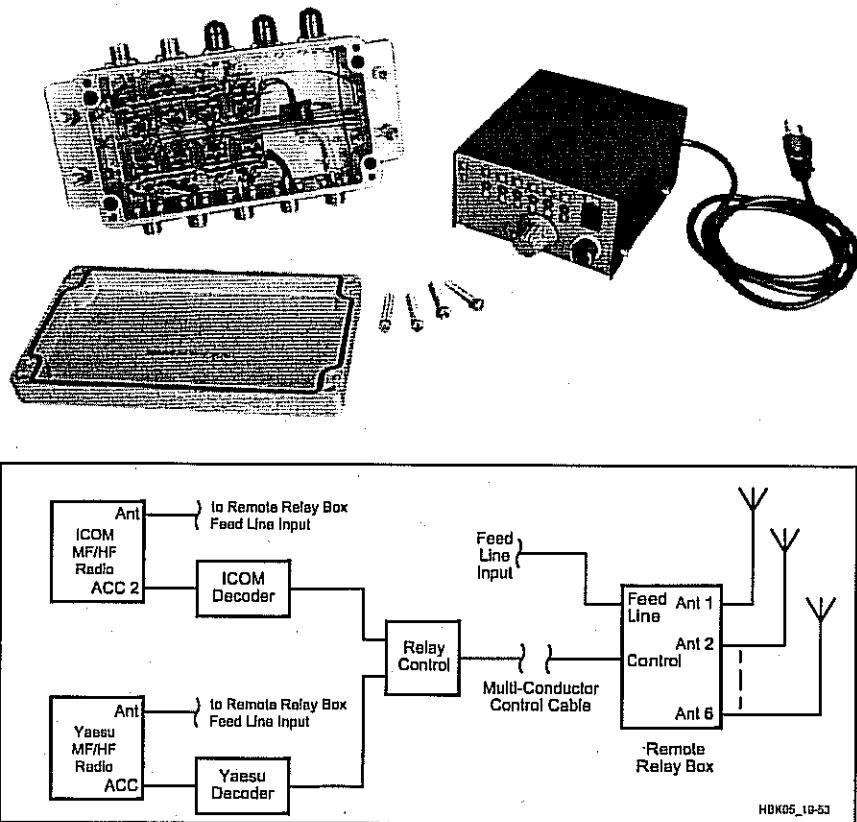


Fig 19.48—Block diagram of the remotely controlled automatic antenna switch.